LTC8631, LTC8632, LTC8634
7MHz, High Slew Rate, RRIO, CMOS Amplifier

General Description

The LTC863x family of single-, dual-, and quad- channel operational amplifiers represents a new generation of general-purpose, low-power op-amps. Featuring rail- to-rail input and output (RRIO) swings, low quiescent current (typical 700 µA) combined with a wide bandwidth (7 MHz) makes this family very attractive for a variety of battery-powered applications that require a good balance between cost and performance, such as motor phase current sensing, photodiode amplification, barcode scanners and white goods. The low input bias current supports these amplifiers to be used in applications with mega-ohm source impedances. The robust design of the LTC863x amplifiers provides ease-of-use to the circuit designer: unity-gain stability with capacitive loads of up to 500 pF, integrated RF/EMI rejection filter, no phase reversal in overdrive conditions, and high electro-static discharge (ESD) protection (3 kV HBM). The LTC863x amplifiers are optimized for operation at voltages as low as +2.3 V (± 1.15 V) and up to +5.5 V (± 2.75 V) over the extended temperature range of −40 ℃ to +125 ℃.

The LTC8631 (single) is available in SOT23-5L package. The LTC8632 (dual) is offered in both SOIC-8L, DFN-8L and MSOP8L packages. The quad-channel LTC8634 is offered in 14- lead SOIC package.

Features and Benefits

- Wide Unity-Gain Bandwidth: 7 MHz
- High Slew Rate: 10 V/µs
- Fast Settling: 0.3 µs to 0.1%
- Low Input Offset Voltage: ± 0.7 mV
- Single 2.3 V to 5.5 V Power Supply Range
- Rail-to-Rail Input and Output
- Internal RF/EMI Filter
- Low Supply Current: 700 µA at 5V Supply Per Amplifier
- Extended Temperature Range: −40℃ to +125℃

Applications

- Motor Phase Current Sense
- Photodiode Amplification
- Active Filters
- Driving A/D Converters
- Portable Equipment
- Battery-Powered Instrumentation

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Table of Content

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Ordering Information[1]

Part Number	Package Type	Package Quantity	ECO Class[2]	Mark Code[3]
LTC8631XT5/R6	SOT23-5L	Tape and Reel, 3 000	Green (RoHS & no Sb/Br)	C31
LTC8632XS8/R8	SOIC-8L	Tape and Reel, 4 000	Green (RoHS & no Sb/Br)	C32
LTC8632XF8/R6	DFN2x2-8L	Tape and Reel, 3 000	Green (RoHS & no Sb/Br)	C32
LTC8632XV8/R6	MSOP-8L	Tape and Reel, 4 000	Green (RoHS & no Sb/Br)	C32
LTC8634XS14/R5	SOIC-14L	Tape and Reel, 2 500	Green (RoHS & no Sb/Br)	C34

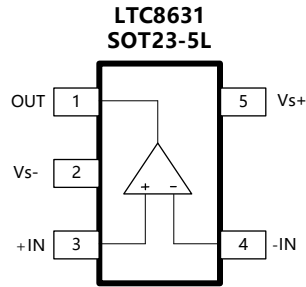* Preview Status (Not for MP stage, pls contact with us if you have request)

(1) Please contact to your Linearin representative for the latest availability information and product content details.

(2) Eco Class - The planned eco-friendly classification: Pb-Free (RoHS) or Green (RoHS & Halogen Free).
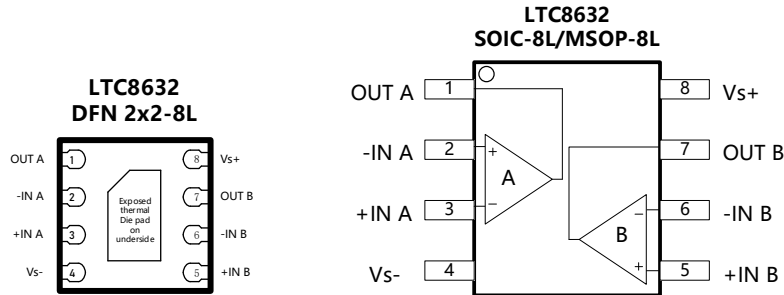
(3) There may be multiple device markings, a varied marking character of "x" , or additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

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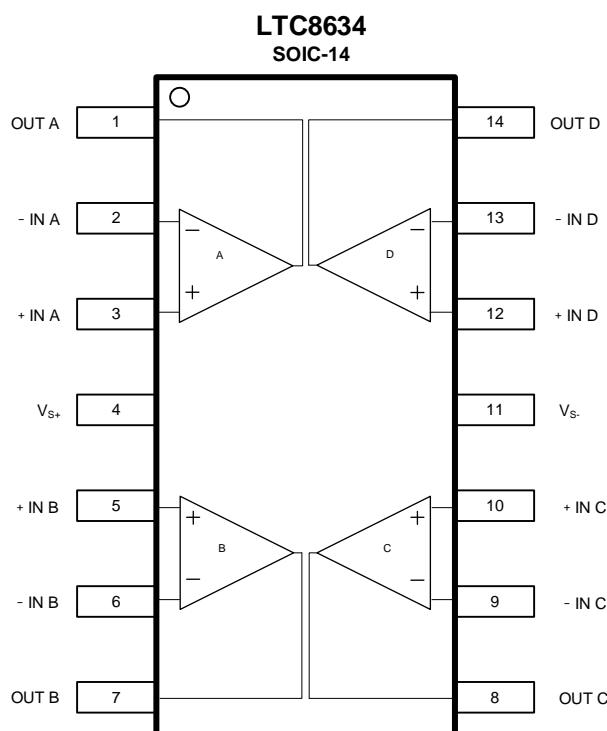
Pin Configuration (Top View)

LTC8631
SOT23-5L

PIN Name	SOT23-5L	Description
OUT	1	Amplifier output.
V_{s-}	2	Negative power supply. It is normally tied to ground. It can also be tied to a voltage other than ground as long as the voltage between V_{S+} and V_{S-} is from 2.3 V to 5.5 V.
–IN	3	Inverting input of the amplifier. The voltage range is from (V_{S-} – 0.1 V) to (V_{S+} + 0.1 V).
+IN	4	Non–inverting input of the amplifier. This pin has the same voltage range as –IN.
V_{s+}	5	Positive power supply. The voltage is from 2.3 V to 5.5 V. Split supplies are possible as long as the voltage between V_{S+} and V_{S-} is from 2.3 V to 5.5 V.

LTC8632
SOIC-8L/MSOP-8L

LTC8632
DFN 2x2-8L

PIN Name	SOIC-8L / MSOP-8L / DFN2x2-8L	Description
OUT A	1	Amplifier A output.
–IN A	2	Inverting input A of the amplifier. The voltage range is from (V_{S-} – 0.1 V) to (V_{S+} + 0.1 V).
+IN A	3	Non–inverting input of the amplifier. This pin has the same voltage range as –IN A.
V_{s-}	4	Negative power supply. It is normally tied to ground. It can also be tied to a voltage other than ground as long as the voltage between V_{S+} and V_{S-} is from 2.3 V to 5.5 V.
+IN B	5	Non–inverting input of the amplifier. This pin has the same voltage range as –IN B.
–IN B	6	Inverting input B of the amplifier. The voltage range is from (V_{S-} – 0.1 V) to (V_{S+} + 0.1 V).
OUT B	7	Amplifier B output.
V_{s+}	8	Positive power supply. The voltage is from 2.3 V to 5.5 V. Split supplies are possible as long as the voltage between V_{S+} and V_{S-} is from 2.3 V to 5.5 V.

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LTC8634
SOIC-14

PIN Name	SOIC-14L	Description
OUT A	1	Amplifier A output.
–IN A	2	Inverting input A of the amplifier. The voltage range is from (V_{S-} – 0.1 V) to (V_{S+} + 0.1 V).
+IN A	3	Non-inverting input of the amplifier. This pin has the same voltage range as –IN A.
V_{s+}	4	Positive power supply. The voltage is from 2.3 V to 5.5 V. Split supplies are possible as long as the voltage between V_{S+} and V_{S-} is from 2.3 V to 5.5 V.
+IN B	5	Non-inverting input of the amplifier. This pin has the same voltage range as –IN B.
–IN B	6	Inverting input B of the amplifier. The voltage range is from (V_{S-} – 0.1 V) to (V_{S+} + 0.1 V).
OUT B	7	Amplifier B output.
OUT C	8	Amplifier C output.
–IN C	9	Inverting input C of the amplifier. The voltage range is from (V_{S-} – 0.1 V) to (V_{S+} + 0.1 V).
+IN C	10	Non-inverting input of the amplifier. This pin has the same voltage range as –IN C.
V_{s-}	11	Negative power supply. It is normally tied to ground. It can also be tied to a voltage other than ground as long as the voltage between V_{S+} and V_{S-} is from 2.3 V to 5.5 V.
+IN D	12	Non-inverting input of the amplifier. This pin has the same voltage range as –IN D.
–IN D	13	Inverting input D of the amplifier. The voltage range is from (V_{S-} – 0.1 V) to (V_{S+} + 0.1 V).
OUT D	14	Amplifier D output.

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Limiting Value

In accordance with the Absolute Maximum Ratin System (IEC60134).

Parameter	Absolute Maximum Rating
Supply Voltage, V_{S+} to V_{S-}	10 V
Signal Input Terminals: Voltage	V_{S-} − 0.5 V to V_{S+} + 0.5 V
Signal Input Terminals: Current	± 10 mA
Output Short-Circuit	Continuous
Storage Temperature Range, T_{sta}	−65 °C to +150 °C
Junction Temperature, T_J	150 °C
Lead Temperature Range (Soldering 10 sec)	260 °C

ESD Ratings

Parameter	Level	UNIT
Human body model (HBM), per ESDA/JEDEC JS-001-2023 [1]	$\pm$3 000	V
Machine Model (MM) , per JESD22-A115C-2010	$\pm$150	V

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process. Manufacturing with less than 500-V HBM is possible if necessary precautions are taken.

Thermal Information

Thermal Metric		Package	Level	Unit
θ_{JA}	Package Thermal Resistance	SOT23-5L	190	°C/W
		SOIC-8L	125	
		MSOP-8L	216	
		DFN2x2-8L	94	
		SOIC-14L	115	

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Electrical Characteristics

V_S = 5.0 V, T_A = + 25 °C, V_{CM} = V_S/2, V_O = V_S /2, and R_L = 10 kΩ connected to V_S/2, unless otherwise noted.

Parameter	Symbol	Conditions	Min.	Typ.	Max.	Unit
OFFSET VOLTAGE						
Input offset voltage	V_{OS}			±0.7	±2.5	mV
Offset voltage drift	V_{OS} TC	T_A = –40 to +125 °C		±1		µV/°C
Power supply rejection ratio	PSRR	V_S = 2.0 to 5.5 V, V_{CM} < V_{S+} –2 V	90	106		dB
		T_A = –40 to +125 °C	85			
INPUT BIAS CURRENT						
Input bias current	I_B			1		pA
		T_A = +85 °C		150		
		T_A = +125 °C		900		
Input offset current	I_{OS}			1		pA
NOISE						
Input voltage noise density	e_n	f = 10 kHz		35		nV/√Hz
INPUT VOLTAGE						
Common–mode voltage range	V_{CM}		V_{S-} – 0.1		V_{S+} + 0.1	V
Common–mode rejection ratio	CMRR	V_S = 5.5 V, V_{CM} = –0.1 to 5.6 V	72	85		dB
		V_S = 5.5 V, V_{CM} = 0 to 3.4 V, T_A = –40 to +125 °C	85			
		V_S = 2.3 V, V_{CM} = –0.1 to 2.4 V	70	82		
		V_S = 2.3 V, V_{CM} = 0 to 0.7 V, T_A = –40 to +125 °C	76			
OPEN–LOOP GAIN						
Open–loop voltage gain	A_{VOL}	R_L = 50 kΩ, V_O = 0.05 to 3.5 V	93	102		dB
		R_L = 50 kΩ, V_O = 0.05 to 3.5 V T_A = –40 to +125 °C	84			
		R_L = 2kΩ, V_O = 0.15 to 3.5 V	91	100		
		R_L = 2kΩ, V_O = 0.15 to 3.5 V T_A = –40 to +125 °C	81			
FREQUENCY RESPONSE						
Gain bandwidth product	GBW			7		MHz
Slew Rate	SR	G = +1, C_L = 100 pF, V_O = 1.5 to 3.5 V		10		V/µs
Overload recovery time	T_{OR}	V_{IN} x Gain > V_S		0.3		µs
OUTPUT						
High output voltage swing	V_{OH}	R_L = 10 kΩ	V_{S+} – 8	V_{S+} – 5		mV
		R_L = 600 Ω	V_{S+} – 180	V_{S+} – 140		
Low output voltage swing	V_{OL}	R_L = 10 kΩ		V_{S-} +5	V_{S-} +7	mV
		R_L = 600 Ω		V_{S-} +80	V_{S-} +90	

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Electrical Characteristics (Cont.)

V_S = 5.0 V, T_A = + 25 °C, V_{CM} = V_S/2, V_O = V_S /2, and R_L = 10 kΩ connected to V_S/2, unless otherwise noted.

Parameter	Symbol	Conditions	Min.	Typ.	Max.	Unit
Short-circuit current	I_{source}	R_L = 10Ω		50		mA
	I_{sink}			75		
POWER SUPPLY						
Operating supply voltage	V_S	T_A = –40 to +125 °C	2.3		5.5	V
Quiescent current (per amplifier)	I_Q	V_S = 2.5 V		600	700	µA
		V_S = 5.0 V		700	850	

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Typical Characteristics

At T_A = 25℃, V_S = 5.0 V, V_{CM} = V_S / 2 and R_L = 10 kΩ connected to V_S / 2, unless otherwise noted.
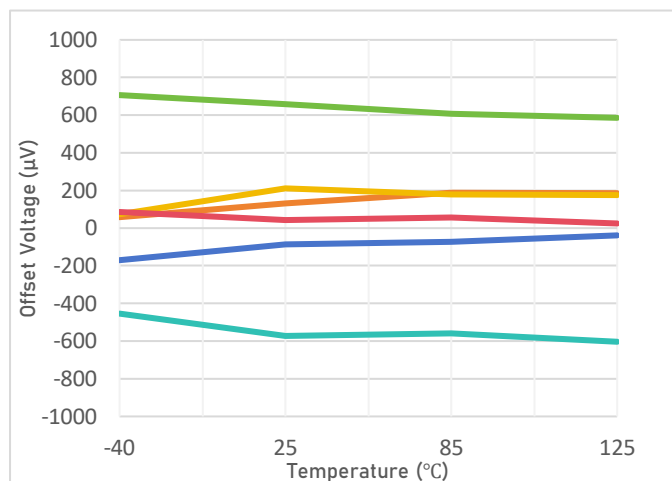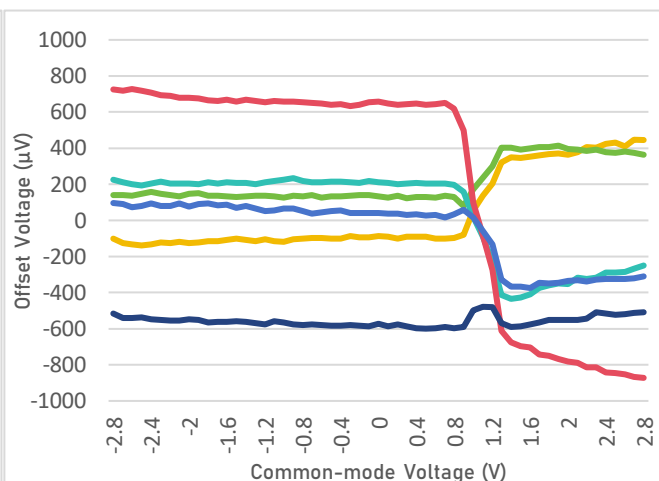
Figure 1. Offset Voltage vs Temperature

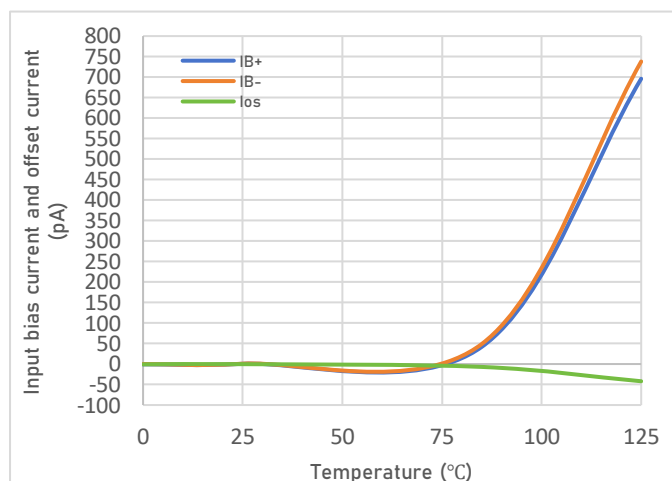Figure 2. Offset Voltage vs Common-mode Voltage
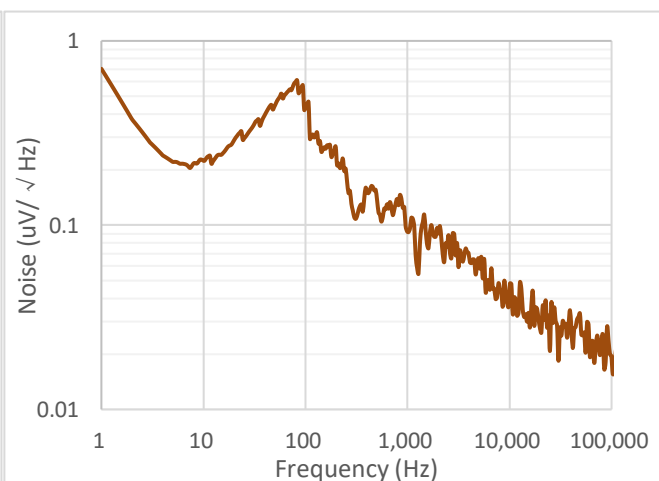
Figure 3. Input Bias Current vs Temperature

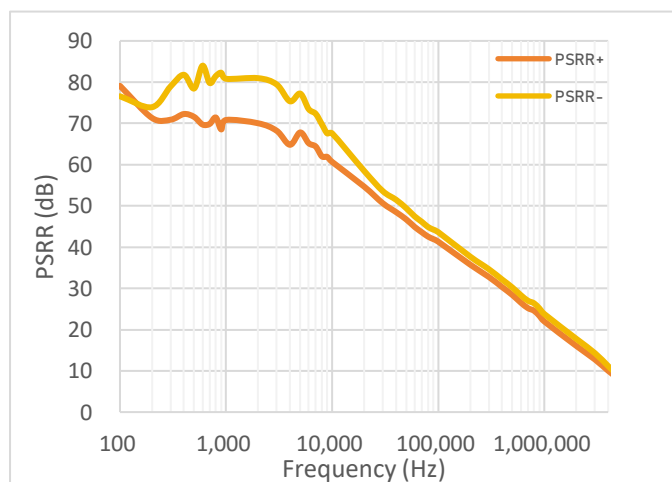Figure 4. Input Voltage Noise Spectral Density vs Frequency

Figure 5. PSRR vs Frequency

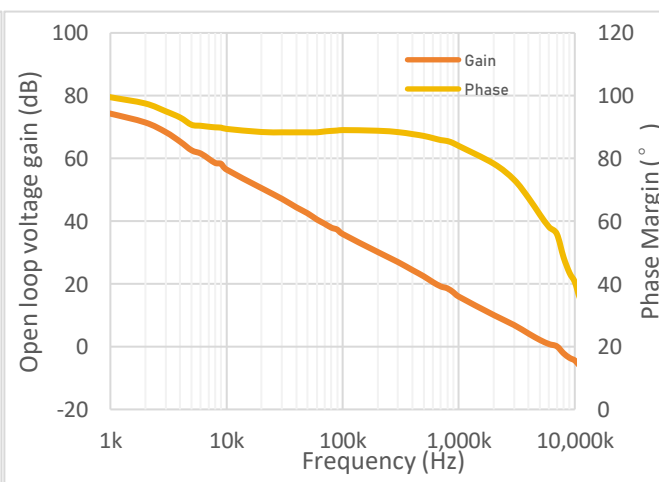Figure 6. Open Loop Gain and Phase vs Frequency

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Typical Characteristics (Cont.)

At T_A = 25℃, V_S = 5.0 V, V_{CM} = V_S / 2 and R_L = 10 kΩ connected to V_S / 2, unless otherwise noted.
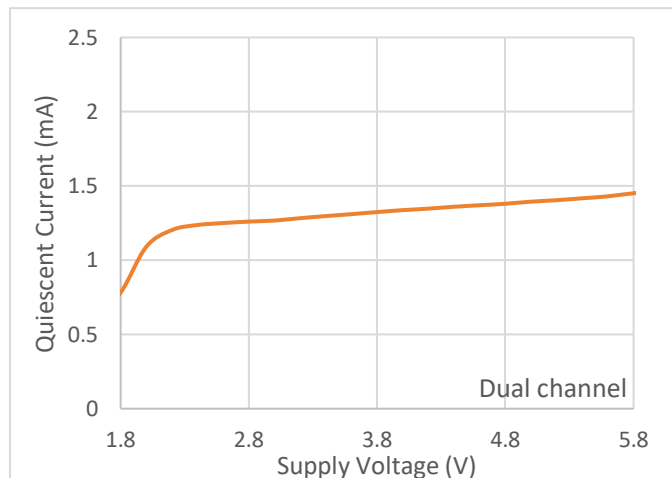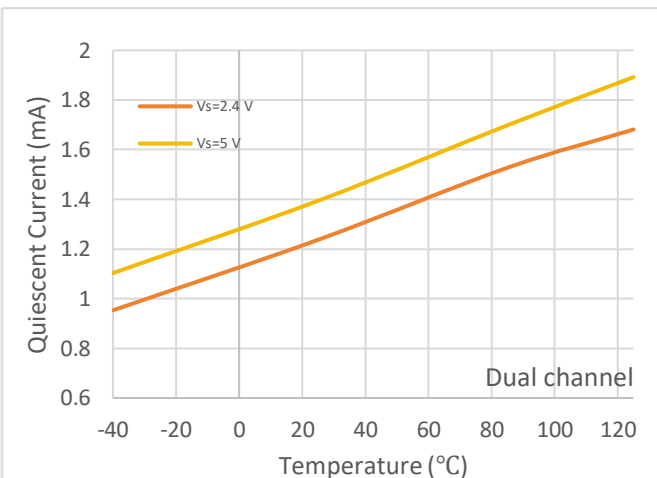

Figure 7. Quiescent Current vs Supply Voltage
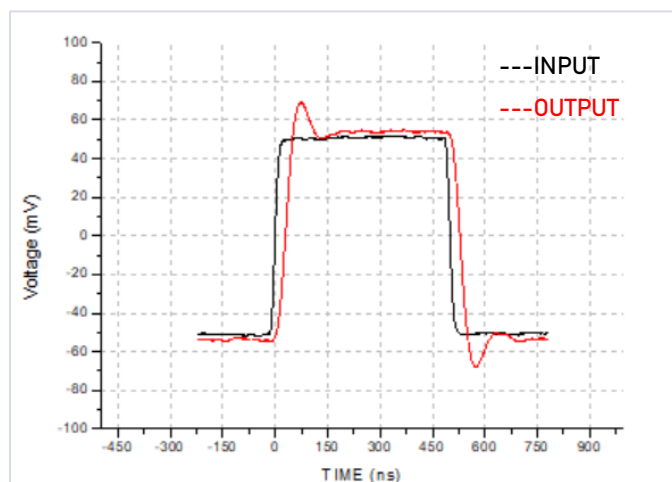

Figure 8. Quiescent Current vs Temperature

Figure 9. Small Signal Step Response

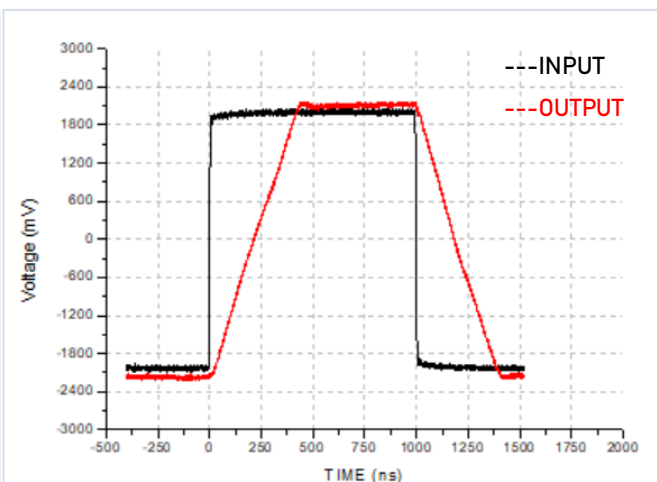Figure 10. Large Signal Step Response

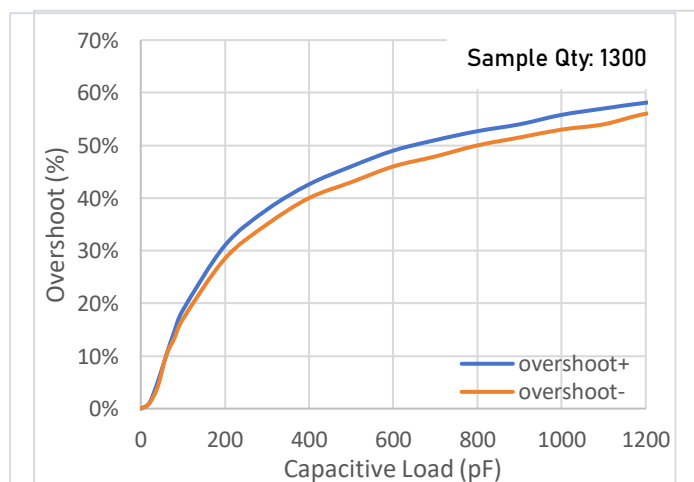Figure 11. Small Signal Overshoot vs Capacitive Load
G= +1V/V, V_{OUT} = 100 mV_{P-P}

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Detailed Description

The LTC863x is a family of low-power, rail-to-rail input and output operational amplifiers specifically designed for portable applications. These devices operate from 2.3 V to 5.5 V at the temperature range of –40 ℃ to +125 ℃, are unity-gain stable, and suitable for a wide range of general-purpose applications. The class AB output stage is capable of driving ≤ 10 kΩ loads connected to any point between V_{S+} and ground. The input common-mode voltage range includes both rails, and allows the LTC863x family to be used in virtually any single supply application. Rail-to-rail input and output swing significantly increases dynamic range, especially in low-supply applications, and makes them ideal for driving sampling analog-to-digital converters (ADCs).

The LTC863x features 7 MHz bandwidth and 10 V/µs slew rate with only 700 µA supply current per amplifier, providing good ac performance at very low power consumption. DC applications are also well served with low input bias current, and an input offset voltage of 0.7 mV typically. The typical offset voltage drift is 1 µV/℃, over the full temperature range the input offset voltage changes only 100 µV (0.7 mV to 0.8 mV).

Operating Voltage

The LTC863x family is optimized for operation at voltages as low as +2.3 V ($\pm$1.15 V) and up to +5.5 V ($\pm$2.75 V). In addition, many specifications apply from –40 ℃ to +125 ℃. Parameters that vary significantly with operating voltages or temperature are illustrated in the Typical Characteristics graphs.

NOTE: Supply voltages (V_{S+} to V_{S-}) higher than +10 V can permanently damage the device.

Rail to rail input

The input common-mode voltage range of the LTC863x series extends 100-mV beyond the negative and positive supply rails. This performance is achieved with a complementary input stage: an N-channel input differential pair in parallel with a P-channel differential pair. The N-channel pair is active for input voltages close to the positive rail, typically V_{S+}–1.4 V to the positive supply, whereas the P-channel pair is active for inputs from 100-mV below the negative supply to approximately V_{S+}–1.4 V. There is a small transition region, typically V_{S+}–1.2 V to V_{S+}–1 V, in which both pairs are on. This 200-mV transition region can vary up to 200-mV with process variation. Thus, the transition region (both stages on) can range from V_{S+}–1.4 V to V_{S+}–1.2 V on the low end, up to V_{S+}–1 V to V_{S+}–0.8 V on the high end. Within this transition region, PSRR, CMRR, offset voltage, offset drift, and THD can be degraded compared to device operation outside this region.

The typical input bias current of the LTC863x during normal operation is approximately 1 pA. In overdriven conditions, the bias current can increase significantly. The most common cause of an overdriven condition occurs when the operational amplifier is outside of the linear range of operation. When the output of the operational amplifier is driven to one of the supply rails, the feedback loop requirements cannot be satisfied and a differential input voltage develops across the input pins. This differential input voltage results in activation of parasitic diodes inside the front-end input chopping switches that combine with electromagnetic interference (EMI) filter resistors to create the equivalent circuit. Notice that the input bias current remains within specification in the linear region.

Input EMI filter and clamp circuit

Figure 1 shows the input EMI filter and clamp circuit. The LTC863x op-amps have internal ESD protection diodes (D1, D2, D3, and D4) that are connected between the inputs and each supply rail. These diodes protect the input transistors in the event of electrostatic discharge and are reverse biased during normal operation. This protection scheme allows voltages as high as approximately 500-mV beyond the rails to be applied at the input of either terminal without causing permanent damage. These ESD protection current-steering diodes also provide in-circuit, input overdrive protection, as long as the current is limited to

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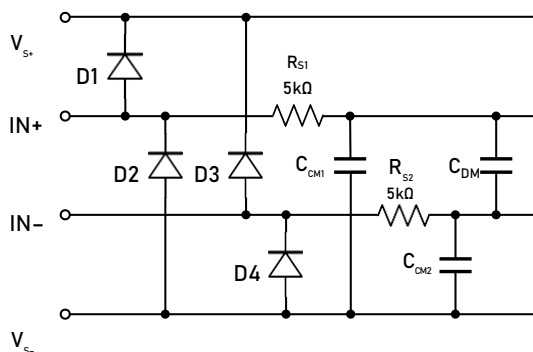20 mA as stated in the Absolute Maximum Ratings.

Figure 1. Input EMI Filter and Clamp Circuit

Operational amplifiers vary in susceptibility to EMI. If conducted EMI enters the operational amplifier, the dc offset at the amplifier output can shift from its nominal value when EMI is present. This shift is a result of signal rectification associated with the internal semiconductor junctions. Although all operational amplifier pin functions can be affected by EMI, the input pins are likely to be the most susceptible. The EMI filter of the LTC863x family is composed of two 5 kΩ input series resistors (R_{S1} and R_{S2}), two common-mode capacitors (C_{CM1} and C_{CM2}), and a differential capacitor (C_{DM}). These RC networks set the −3 dB low-pass cutoff frequencies at 35 MHz for common-mode signals, and at 22 MHz for differential signals.

Rail to rail output

Designed as a micro-power, low-noise operational amplifier, the LTC863x delivers a robust output drive capability. A class AB output stage with common-source transistors is used to achieve full rail-to-rail output swing capability. For resistive loads up to 100 kΩ, the output swings typically to within 5-mV of either supply rail regardless of the power-supply voltage applied. Different load conditions change the ability of the amplifier to swing close to the rails. For resistive loads up to 600 Ω, the output swings typically to within 140 mV of the positive supply rail and within 80 mV of the negative supply rail.

Capacitive load and stability

The LTC863x family can safely drive capacitive loads of up to 500 pF in any configuration. As with most amplifiers, driving larger capacitive loads than specified may cause excessive overshoot and ringing, or even oscillation. A heavy capacitive load reduces the phase margin and causes the amplifier frequency response to peak. Peaking corresponds to overshooting or ringing in the time domain. Therefore, it is recommended that external compensation be used if the LTC863x op-amps must drive a load exceeding 500 pF. This compensation is particularly important in the unity-gain configuration, which is the worst case for stability.

A quick and easy way to stabilize the op-amp for capacitive load drive is by adding a series resistor, R_{ISO}, between the amplifier output terminal and the load capacitance, as shown in Figure 2. R_{ISO} isolates the amplifier output and feedback network from the capacitive load. The bigger the R_{ISO} resistor value, the more stable V_{OUT} will be. Note that this method results in a loss of gain accuracy because R_{ISO} forms a voltage divider with the R_L.
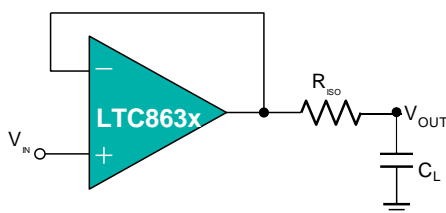
Figure 2. Indirectly Driving Heavy Capacitive Load

An improvement circuit is shown in Figure 3. It provides DC accuracy as well as AC stability. The R_F provides the DC accuracy by connecting the inverting signal with the output.

The C_F and R_{ISO} serve to counteract the loss of phase margin by feeding the high frequency component of the output signal back to the amplifier's inverting input, thereby preserving phase margin in the overall feedback loop.

For no-buffer configuration, there are two other ways to increase the phase margin: (a) by increasing the amplifier's gain, or (b) by placing a capacitor in parallel with the feedback resistor to counteract the parasitic capacitance associated with inverting node.
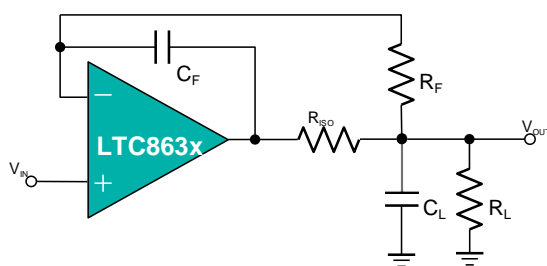

Figure 3. Indirectly Driving Heavy Capacitive Load   with DC Accuracy

Overload recovery

Overload recovery is defined as the time required for the operational amplifier output to recover from a saturated state to a linear state. The output devices of the operational amplifier enter a saturation region when the output voltage exceeds the rated operating voltage, either because of the high input voltage or the high gain. After the device enters the saturation region, the charge carriers in the output device require time to return back to the linear state. After the charge carriers return back to the linear state, the device begins to slew at the specified slew rate. Thus, the propagation delay in case of an overload condition is the sum of the overload recovery time and the slew time. The overload recovery time for the LTC863x family is approximately 0.3 µs.

EMI rejection ratio

Circuit performance is often adversely affected by high frequency EMI. When the signal strength is low and transmission lines are long, an op-amp must accurately amplify the input signals. However, all op-amp pins — the non-inverting input, inverting input, positive supply, negative supply, and output pins — are susceptible to EMI signals. These high frequency signals are coupled into an op-amp by various means, such as conduction, near field radiation, or far field radiation. For example, wires and printed circuit board (PCB) traces can act as antennas and pick up high frequency EMI signals.

Amplifiers do not amplify EMI or RF signals due to their relatively low bandwidth. However, due to the nonlinearities of the input devices, op-amps can rectify these out of band signals. When these high frequency signals are rectified, they appear as a dc offset at the output.

The LTC863x op-amps have integrated EMI filters at their input stage. A mathematical method of measuring EMIRR is

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defined as follows:

EMIRR = 20 log (V_{IN_PEAK} / ΔV_{OS})

Input to output coupling

To minimize capacitive coupling, the input and output signal traces should not be parallel. This helps reduce unwanted positive feedback.

Maximizing performance through proper layout

To achieve the maximum performance of the extremely high input impedance and low offse voltage of the LTC 863x op-amps, care is needed in laying out the circuit board. The PCB surface must remain clean and free of moisture to avoid leakage currents between adjacent traces. Surface coating of the circuit board reduces surface moisture and provides a humidity barrier, reducing parasitic resistance on the board. The use of guard rings around the amplifier inputs further reduces leakag currents. Figure 4 shows proper guard ring configuration and the top view of a surface-mount layout. The guard ring does not need to be a specific width, but it should form a continuous loop around both inputs. By setting the guard ring voltage equal to the voltage at the non-inverting input, parasitic capacitance is minimized as well. For further reduction of leakage currents, components can be mounted to the PCB using Teflon standoff insulators.
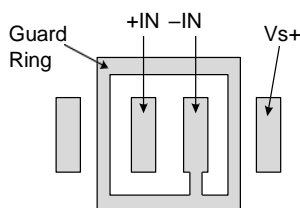

Figure 4. Use a guard ring around sensitive pins

Other potential sources of offset error are thermoelectric voltages on the circuit board. This voltage, also called Seebeck voltage, occurs at the junction of two dissimilar metals and is proportional to the temperature of the junction. The most common metallic junctions on a circuit board are solder-to-board trace and solder-to-component lead. If the temperature of the PCB at one end of the component is different from the temperature at the other end, the resulting Seebeck voltages are not equal, resulting in a thermal voltage error.

This thermocouple error can be reduced by using dummy components to match the thermoelectric error source. Placing the dummy component as close as possible to its partner ensures both Seebeck voltages are equal, thus canceling the thermocouple error. Maintaining a constant ambient temperature on the circuit board further reduces this error. The use of a ground plane helps distribute heat throughout the board and reduces EMI noise pickup.

Typical Application Circuit

Active filter

The LTC863x family is well-suited for active filter applications that require a wide bandwidth, fast slew rate, single-supply operational amplifier. Figure 5 shows a 500 kHz, second-order, low-pass filter using the multiple-feedback (MFB) topology. The components have been selected to provide a maximally-flat Butterworth response. Beyond the cut-off frequency, roll-off is –40 dB/dec. The Butterworth response is ideal for applications that require predictable gain characteristics, such as the anti-aliasing filter used in front of an ADC.
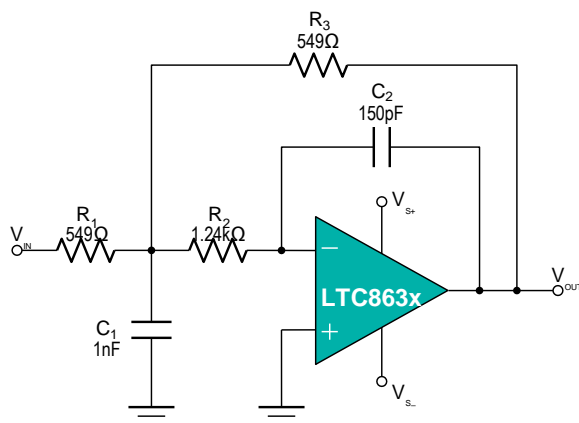

Figure 5. Second-Order, Butterworth, 500-kHz Low- Pass Filter

One point to observe when considering the MFB filter is that the output is inverted, relative to the input. If this inversion is not required, or not desired, a non- inverting output can be achieved through one of these options:

1. adding an inverting amplifier ;
2. adding an additional second-order MFB stage;
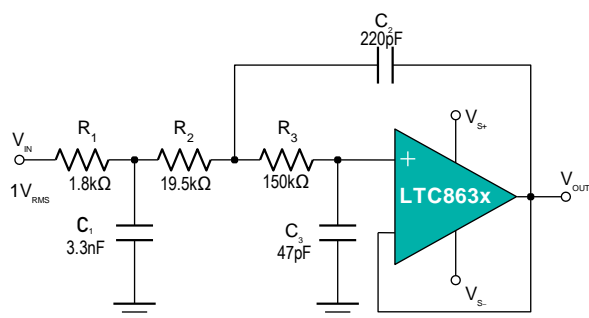3. using a non-inverting filter topology, such as the Sallen-Key (shown in Figure 6).

Figure 6. Configured as a Three-Pole, 20-kHz, Sallen- Key Filter

Motor phase current sensing

The current sensing amplification shown in Figure 7 has a slew rate of $2\pi f V_{PP}$ for the output of sine wave signal, and has a slew rate of $2fV_{PP}$ for the output of triangular wave signal. In most of motor control systems, the PWM frequency is at 10 kHz to 20 kHz, and one cycle time is 100 µs for a 10 kHz of PWM frequency. In current shunt monitoring for a motor phase, the phase current is converted to a phase voltage signal for ADC sampling. This sampling voltage signal must be settled before entering the ADC. As the Figure 7 shown, the total settling time of a current shunt monitor circuit includes: the rising edge delay time (t_{SR}) due to the op-amp's slew rate, and the measurement settling time (t_{SET}). For a 2- shunt solution of motor phase current sensing, if the minimum duty cycle of the PWM is defined at 5%, and the t_{SR} is required at 20% of a total time window for a phase

current monitoring, in case of a 3.3 V motor control system (3.3 V MCU with 12-bit ADC), the op- amp's slew rate should be more than:

3.3V / (100μs× 5% × 20%) = 3.3 V/μs

At the same time, the op-amp's bandwidth should be much greater than the PWM frequency, like 10 time at least.
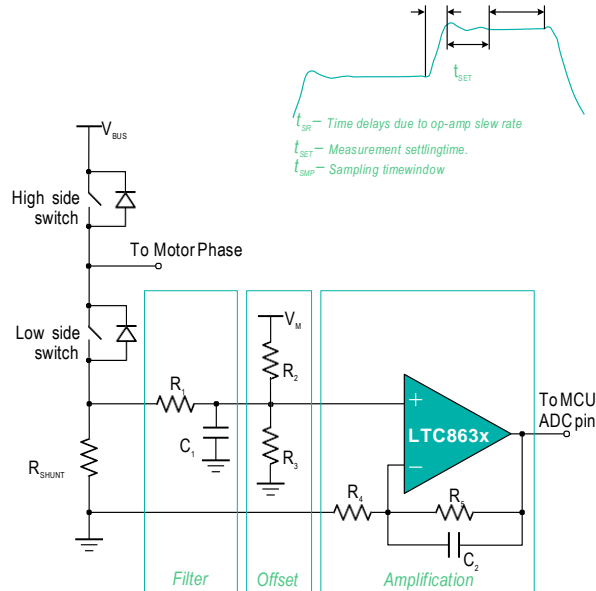
Figure 7. Current Shunt Monitor Circuit

Differential amplifier

The circuit shown in Figure 8 performs the difference function. If the resistors ratios are equal R_4/R_3 = R_2/R_1, then:

$V_{OUT} = (V_p - V_n) × R_2/R_1 + V_{REF}$
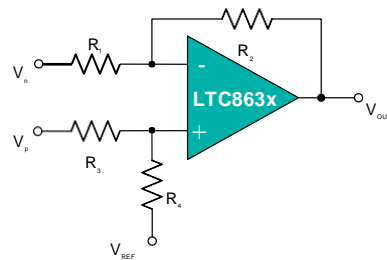
Figure 8. Differential Amplifier

Instrumentation amplifier

$$VOUT = (V1 - V2)\left(1 + \frac{R1}{R2} + \frac{2R1}{RG}\right) + VREF$$
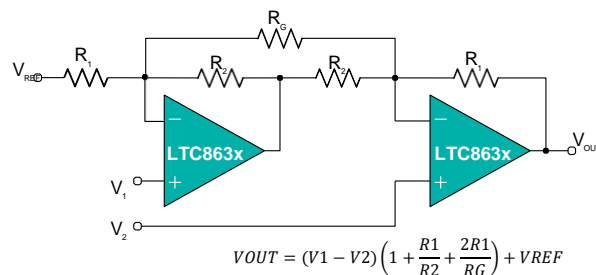
Figure 9. Instrumentation Amplifier

The LTC863x family is well suited for conditioning sensor signals in battery-powered applications. Figure 9 shows a two op-amp instrumentation amplifier, using the LTC863x op-amps. The circuit works well for applications requiring rejection of

common-mode noise at higher gains. The reference voltage (V_{REF}) is supplied by a low-impedance source. In single voltage supply applications, the V_{REF} is typically $V_S/2$.

Buffered chemical sensors
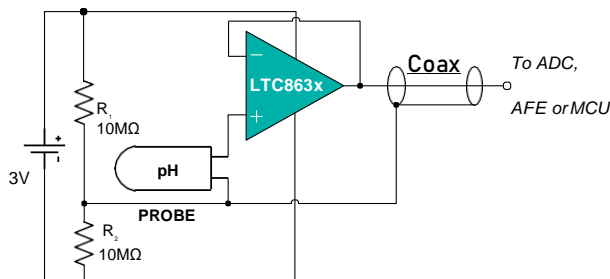
All components contained within the pH probe

Figure 10. Buffered pH Probe

The LTC863x family has input bias current in the pA range. This is ideal in buffering high impedance chemical sensors, such as pH probes. As an example, the circuit in Figure 10 eliminates expansive low-leakage cables that that is required to connect a pH probe (general purpose combination pH probes, e.g Corning 476540) to metering ICs such as ADC, AFE and/or MCU. A LTC863x op-amp and a lithium battery are housed in the probe assembly. A conventional low-cost coaxial cable can be used to carry the op-amp's output signal to subsequent ICs for pH reading.

Tape and Reel Information

REEL DIMENSIONS
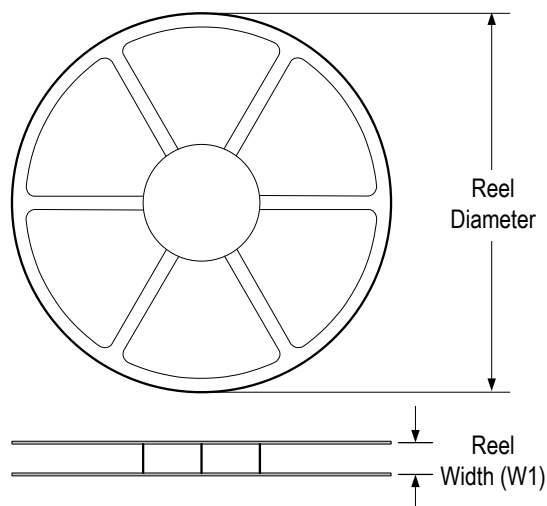
TAPE DIMENSIONS
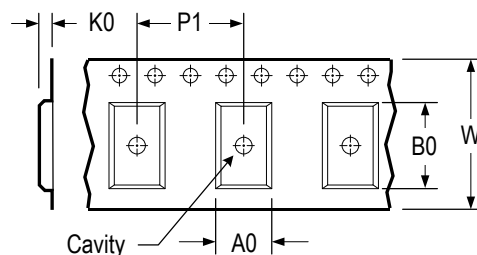
A0	Dimension designed to accommodate the component width
B0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

QUADRANT ASSIGNMENTS FOR PIN 1 ORIETATION IN TAPE
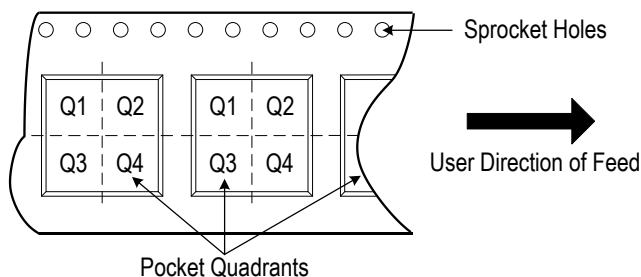
* All dimensions are nominal

Device	Package Type	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin 1 Quadrant
LTC8631XT5/R6	SOT23	5	3 000	178	9.0	3.3	3.2	1.5	4.0	8.0	Q3
LTC8632XS8/R8	SOIC	8	4 000	330	12.4	6.6	5.3	2.0	8.0	12.0	Q1
LTC8632XF8/R6	DFN	8	3 000	178	9.0	2.3	2.3	1.1	4.0	7.9	Q1
LTC8632XV8/R6	MSOP	8	3 000	330	12.4	5.0	3.5	2.0	8.0	12.0	Q1
LTC8634XS14/R5	SOIC	14	2 500	330	12.4	6.5	9.5	2.0	8.0	16.0	Q1

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Package Outlines

DIMENSIONS, SOT23-5L
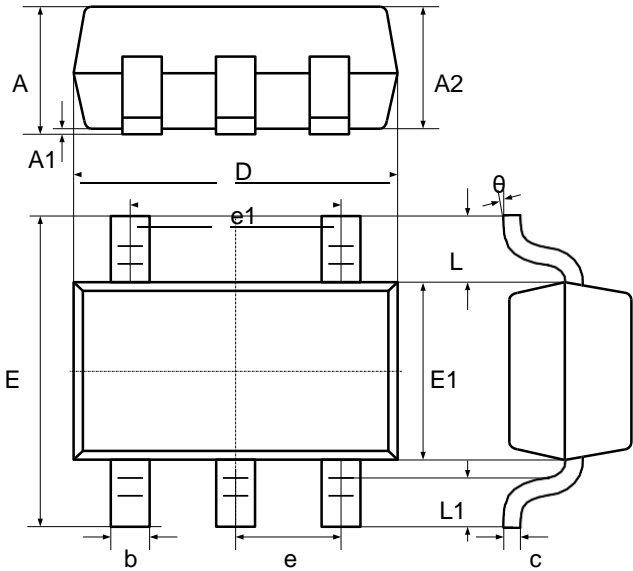
Symbol	Dimensions In Millimeters		Dimensions In Inches	
	Min	Max	Min	Max
A	-	1.25	-	0.049
A1	0.04	0.10	0.002	0.004
A2	1.00	1.20	0.039	0.047
b	0.33	0.41	0.013	0.016
c	0.15	0.19	0.006	0.007
D	2.820	3.02	0.111	0.119
E1	1.50	1.70	0.059	0.067
E	2.60	3.00	0.102	0.118
e	0.95 BSC		0.037 BSC	
e1	1.90 BSC		0.075 BSC	
L	0.60 REF		0.024 REF	
L1	0.30	0.60	0.012	0.024
θ	0°	8°	0°	8°

RECOMMENDED SOLDERING FOOTPRINT, SOT23-5L

$\left(\dfrac{mm}{inches}\right)$

LINEARIN

Package Outlines (cont.)

DIMENSIONS, DFN-8L

SYMBOL	MILLIMETER		
	MIN	NOM	MAX
A	0.700	0.750	0.800
A1	0.000	0.020	0.050
b	0.200	0.250	0.300
b1	0.18REF		
C	0.180	0.200	0.220
D	1.900	2.000	2.100
E	1.900	2.000	2.100
D1	1.100	1.200	1.300
E1	0.600	0.700	0.800
e	0.475	0.500	0.525
L	0.300	0.350	0.400
F	0.280	0.300	0.320
h	0.230	0.280	0.330

RECOMMENDED SOLDERING FOOTPRINT, DFN-8L

SOLDER PASTE EXAMPLE
BASED ON 0.125 mm THICK STENCIL

EXPOSED PAD 9:
87% PRINTED SOLDER COVERAGE BY AREA UNDER PACKAGE
SCALE:25X

Package Outlines (cont.)

DIMENSIONS, SOIC-8L

Symbol	Dimensions In Millimeters		Dimensions In Inches	
	Min	Max	Min	Max
A	1.370	1.670	0.054	0.066
A1	0.070	0.170	0.003	0.007
A2	1.300	1.500	0.051	0.059
b	0.306	0.506	0.012	0.020
C	0.203 TYP.		0.008 TYP.	
D	4.700	5.100	0.185	0.201
E	3.820	4.020	0.150	0.158
E1	5.800	6.200	0.228	0.244
e	1.270 TYP.		0.050 TYP.	
L	0.450	0.750	0.018	0.030
θ	0°	8°	0°	8°

RECOMMENDED SOLDERING FOOTPRINT, SOIC-8L

$8X \frac{(1.55)}{(0.061)}$ MAX

$\frac{5.40}{0.213}$

$\frac{(3.90)}{(0.154)}$ MIN

1

$\frac{(0.60)}{(0.024)}$ MAX 8X

PITCH $\frac{1.270}{0.050}$

$\left(\frac{mm}{inches}\right)$

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Package Outlines (cont.)

DIMENSIONS, MSOP-8L

Symbol	Dimensions In Millimeters		Dimensions In Inches	
	Min	Max	Min	Max
A	0.800	1.100	0.031	0.043
A1	0.050	0.150	0.002	0.006
A2	0.750	0.950	0.030	0.037
b	0.290	0.380	0.011	0.015
C	0.150	0.200	0.006	0.008
D	2.900	3.100	0.114	0.122
E	2.900	3.100	0.114	0.122
E1	4.700	5.100	0.185	0.201
e	0.650 TYP.		0.026 TYP.	
L	0.400	0.700	0.016	0.028
θ	0°	8°	0°	8°
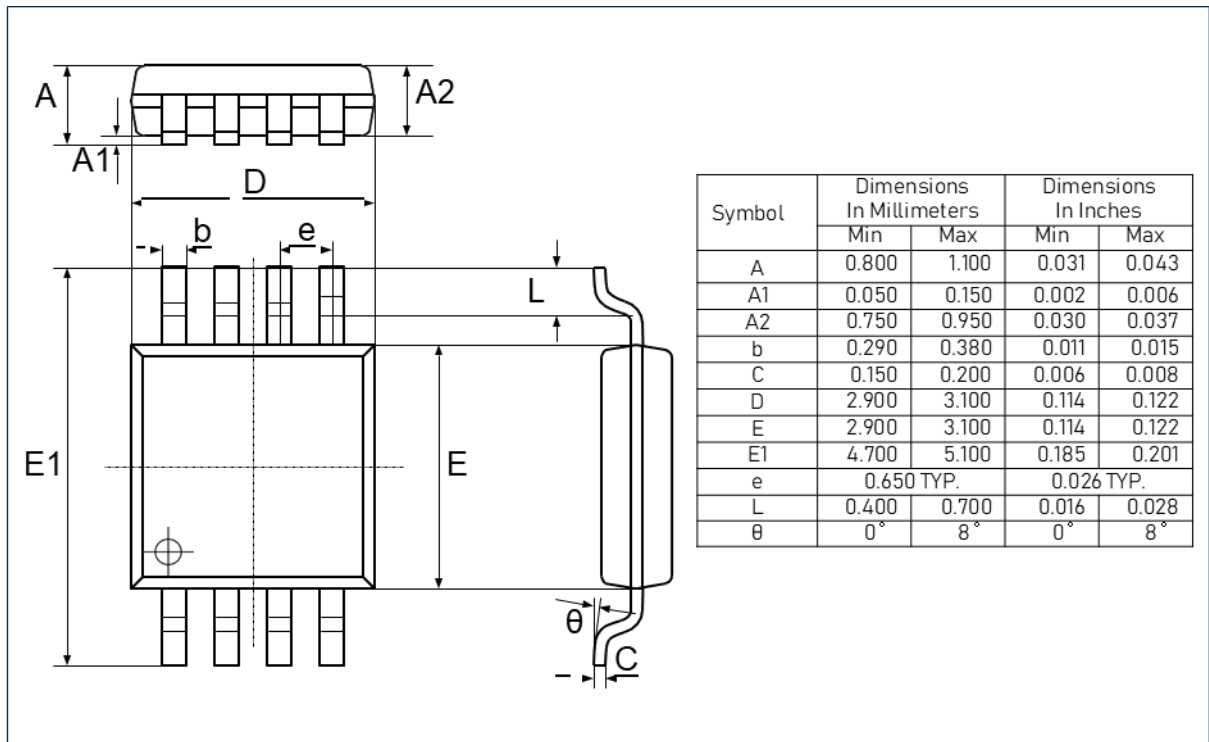
RECOMMENDED SOLDERING FOOTPRINT, MSOP-8L

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Package Outlines (Cont.)

DIMENSIONS, SOIC-14L

Symbol	Dimensions In Millimeters		Dimensions In Inches	
	Min	Max	Min	Max
A	1.450	1.850	0.057	0.073
A1	0.100	0.300	0.004	0.012
A2	1.350	1.550	0.053	0.061
A3	0.550	0.750	0.022	0.030
b	0.406 TYP.		0.016 TYP.	
C	0.203 TYP.		0.008 TYP.	
D	8.630	8.830	0.340	0.348
E	5.840	6.240	0.230	0.246
E1	3.850	4.050	0.152	0.159
e	1.270 TYP.		0.050 TYP.	
L1	1.040 REF.		0.041 REF.	
L	0.350	0.750	0.014	0.030
θ	2°	8°	2°	8°
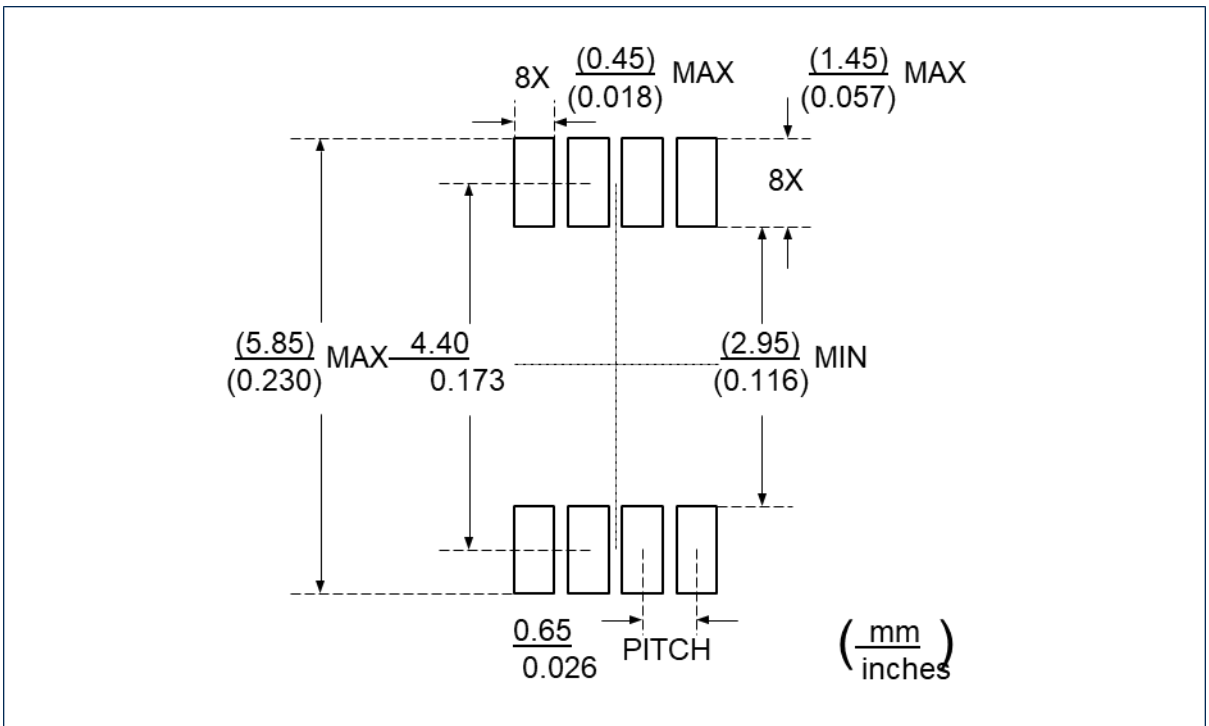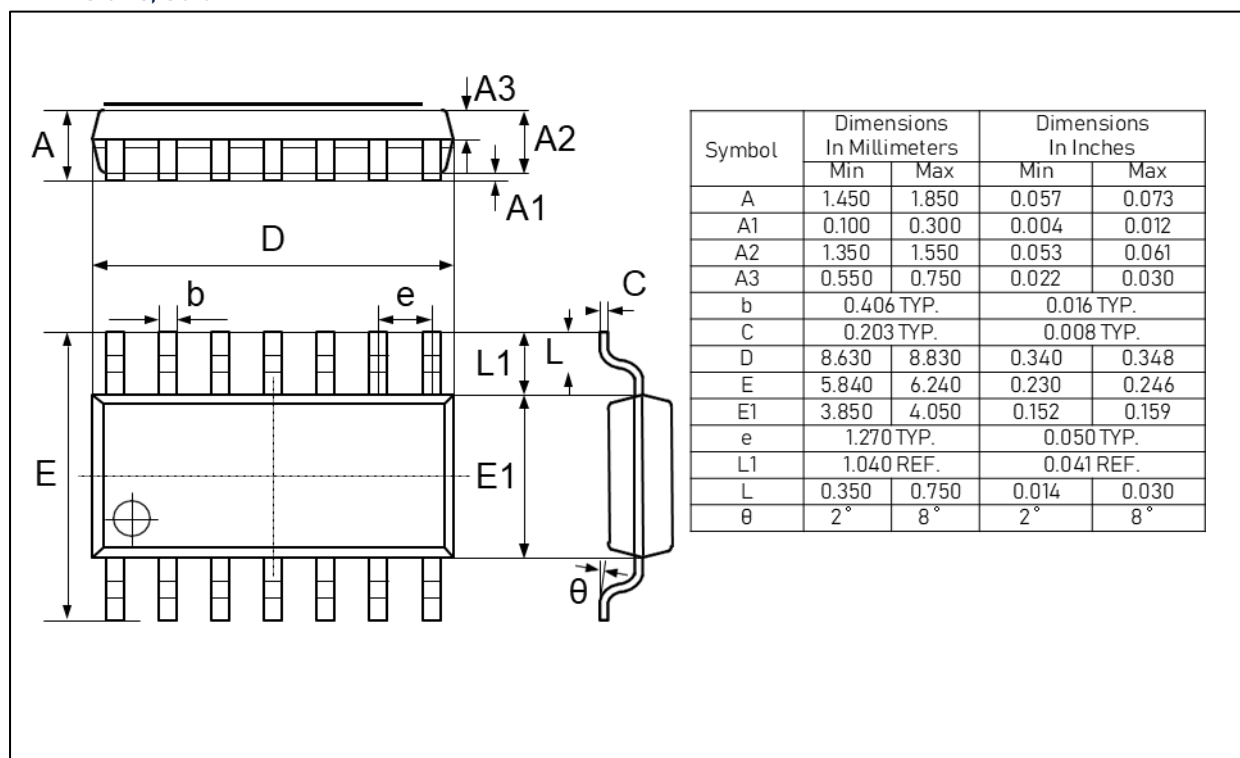
RECOMMENDED SOLDERING FOOTPRINT, SOIC-14L
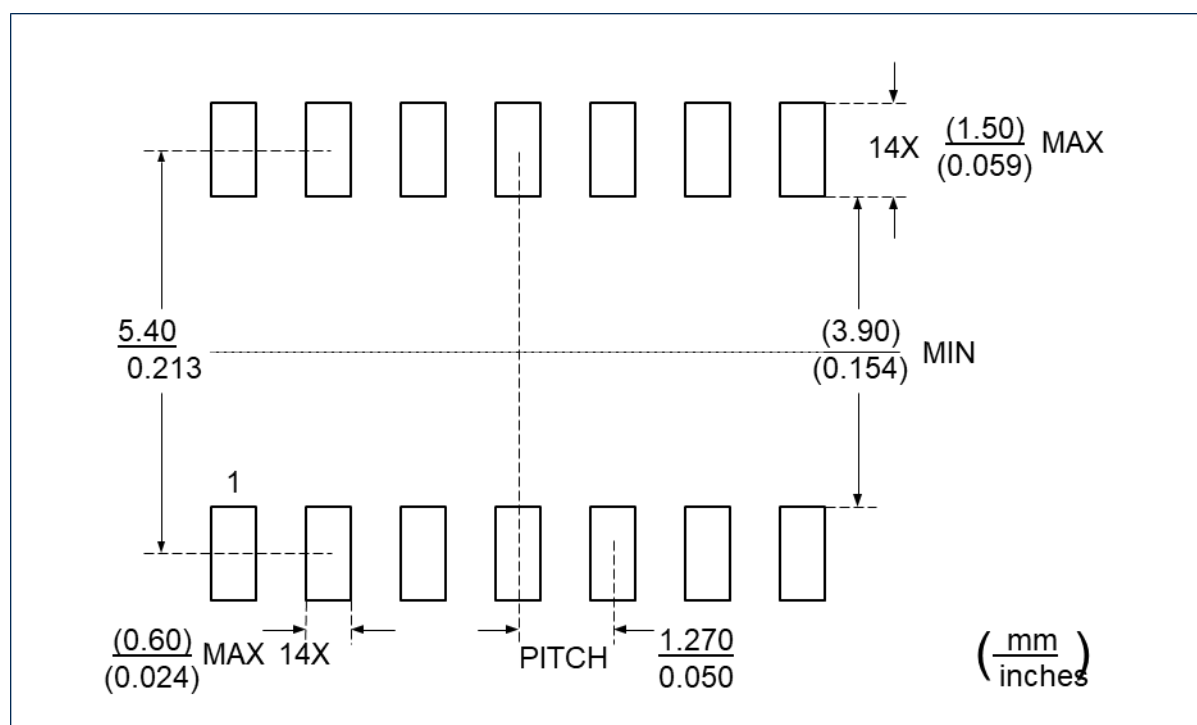
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Important Notice

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For additional product information, or full datasheet, please contact with the Linearin's Sales Department or Representatives.

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